includes, on a mass percent basis, 0.028% of C, 0.24% of Si, 1.62% of Mn, 0.048% of Nb, 0.071% of V, 0.01% of Cu, 0.01% of Ni, and the balance being Fe and incidental impurities.

Kindly replace Paragraph [0061] on Page 15 as follows:

[0050] Fig. 4 shows the relationship between the coiling temperature (hereinafter referred to as "CT" in some cases) and the Nb precipitation ratio. It is understood that the Nb precipitation precipitation ratio is proportional to CT. When CT is more than about 700°C, the Nb precipitation ratio becomes more than about 80%. Hence, CT is preferably controlled to be about 700°C or less to obtain superior toughness. In particular, CT is preferably set to about 600°C or less.

Kindly replace Paragraph [0066] on Page 16 as follows

[0066] In contrast, according to steels I to R, which were outside the invention our conditions, a desired toughness could not be obtained.

Kindly replace Paragraph [0072] on Page 17 as follows:

[0072] According to our examples (steels T to X) of the invention, it was found that the steel microstructure is composed of bainitic ferrite as a primary phase in which $\alpha B \ge 95$ percent by volume is satisfied; the strength is high such that $YS \ge 652$ MPa is satisfied; and the toughness of the mother material and the weld portion are superior, each having a CTOD value of 0.28 mm or more.

Kindly replace Paragraph [0073] on Page 17 as follows:

[0073] In contrast, according to steel Y, since Pcm and the amount of Ca were outside the appropriate region of this invention, the CTOD value of the weld portion was low, and the cleanness of steel was degraded by excessive addition of Ca. Consequently, a desired toughness could not be obtained.

CH 18/18/08